

# Duct Design and Installation

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# Duct Design

- ACCA Manuals J, T, and D or Equivalent

# Proper Design & Selection – Estimate Loads

1. Determine Design Heating Loads
2. Determine Design Cooling Loads –  
Sensible and Latent
3. Determine the airflow required to each  
room

# Proper Design

1. Determine the best locations for the air terminals (registers)

Use ACCA Manual T

2. Design the duct system to the available pressure and minimize the effective length

Use ACCA Manual D or Equivalent

# A Good Duct Design Provides

- Quiet
- Efficient
- Comfort

# Recommended Velocity (in fpm)

Duct Type	Supply		Return	
	Rigid	Flex	Rigid	Flex
Trunk	700	600	600	600
Branch	600	600	400	400
Outlet	Size for Throw			
Return Grille Face			<500	
Filter Grille			<300	

# Efficient

- **FAN WATT DRAW REDUCTION**
- **SUFFICIENT AIRFLOW**
- **LOW DUCT LEAKAGE**
  - SEAL WITH MASTIC OR SNAP-DUCT
  - PUT INSIDE THE CONDITIONED SPACE
- **LOW CONDUCTION LOSS**
  - SHORT RUNS
  - FEWER LARGER DIAMETER RUNS
  - PUT INSIDE THE CONDITIONED SPACE
  - USE METAL DUCT AND FITTINGS

# Comfort

## TEMPERATURE DIFFERENCE BETWEEN ROOMS

< 2 ° F IDEAL

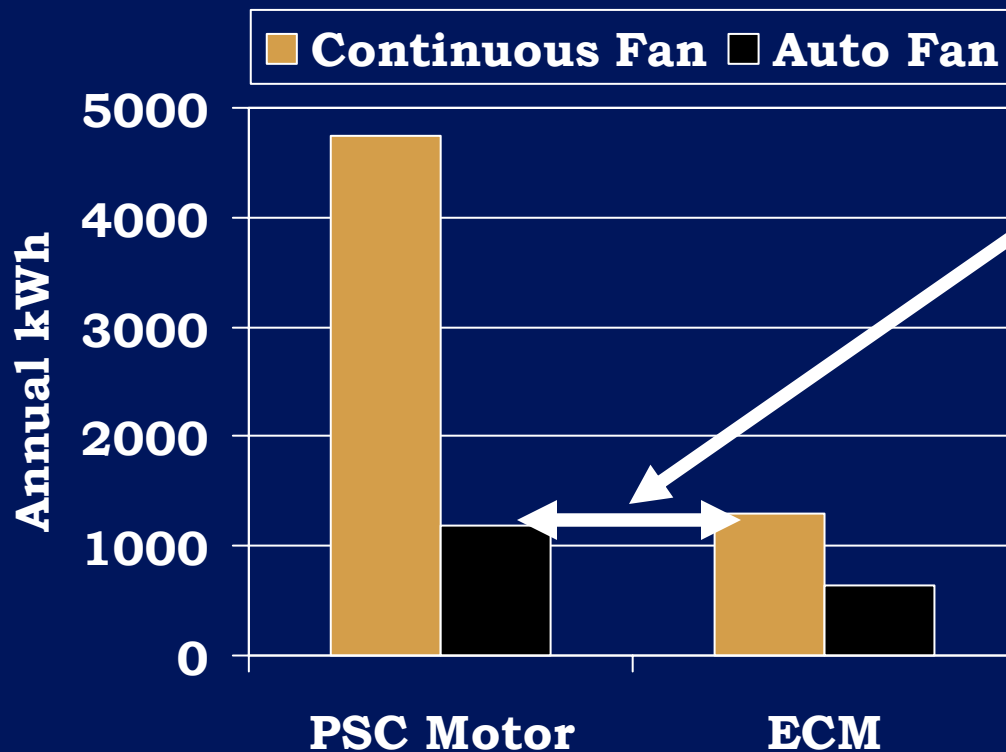
4 ° F MAXIMUM

SO USE A CONTINUOUS FAN?

**NO**



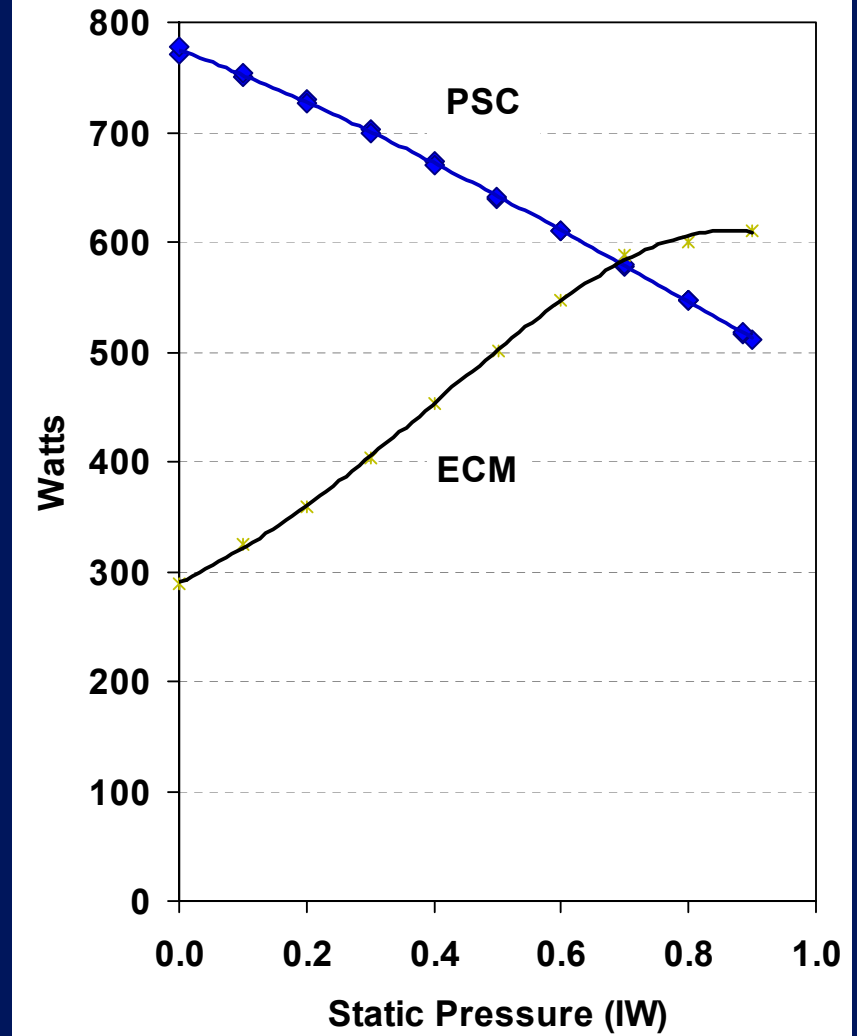
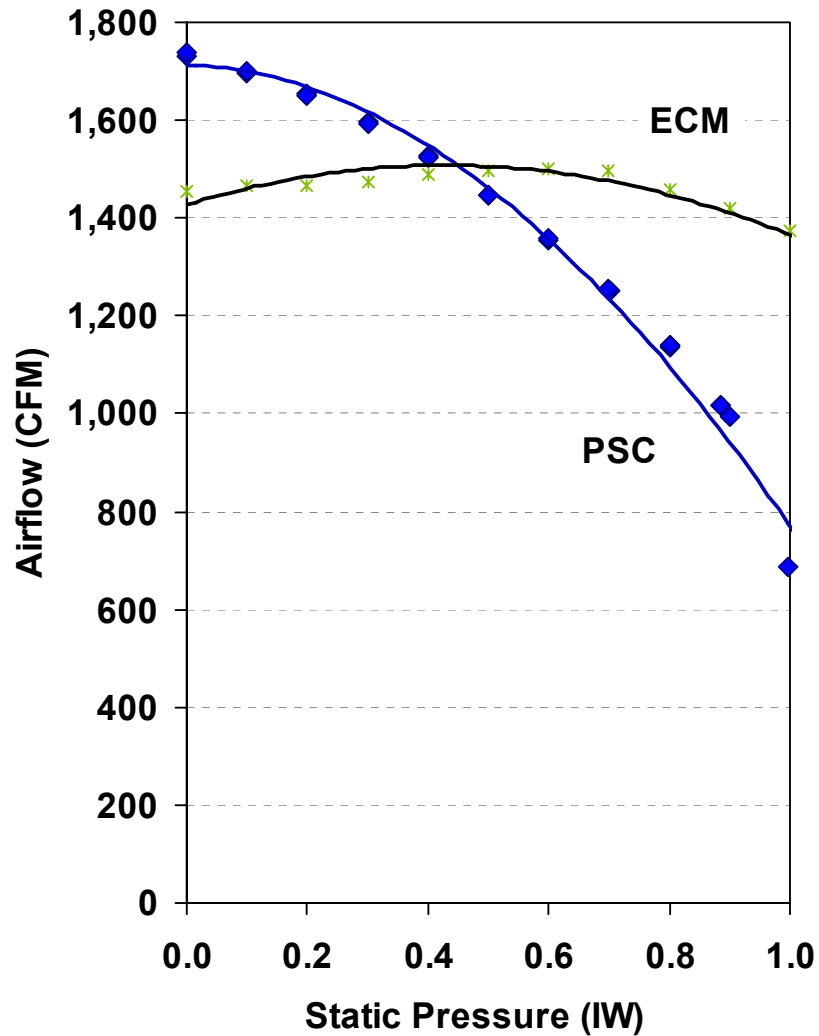
# Why not just add an Electrically Commutated Motor (ECM) and use a continuous fan?



1. An ECM uses as much power running continuously as a PSC motor does running on Auto  
(Scott Pigg, Wisconsin Study)

2. Continuous duct leakage losses and conduction losses
3. ECM motors are not magic – When pressures are too high they can use more electricity and burnout

# ECM Motors Maintain Airflow (up to a point) but can use more watts than a PSC



# **Comfort comes from a designed system**

Duct System Must Be Designed to Deliver Correct Amount of Air to Each Supply Terminal

**AND**

Each Supply Terminal Must Be Carefully Sized and Located

**AND**

Each Supply Terminal Must Be Chosen With Adequate Mixing and Throw

**AND**

There Must Be an Adequate Return Path for Each Supply

# Terminals

- SUPPLY LOCATION (old recommendation)

## PERIMETER

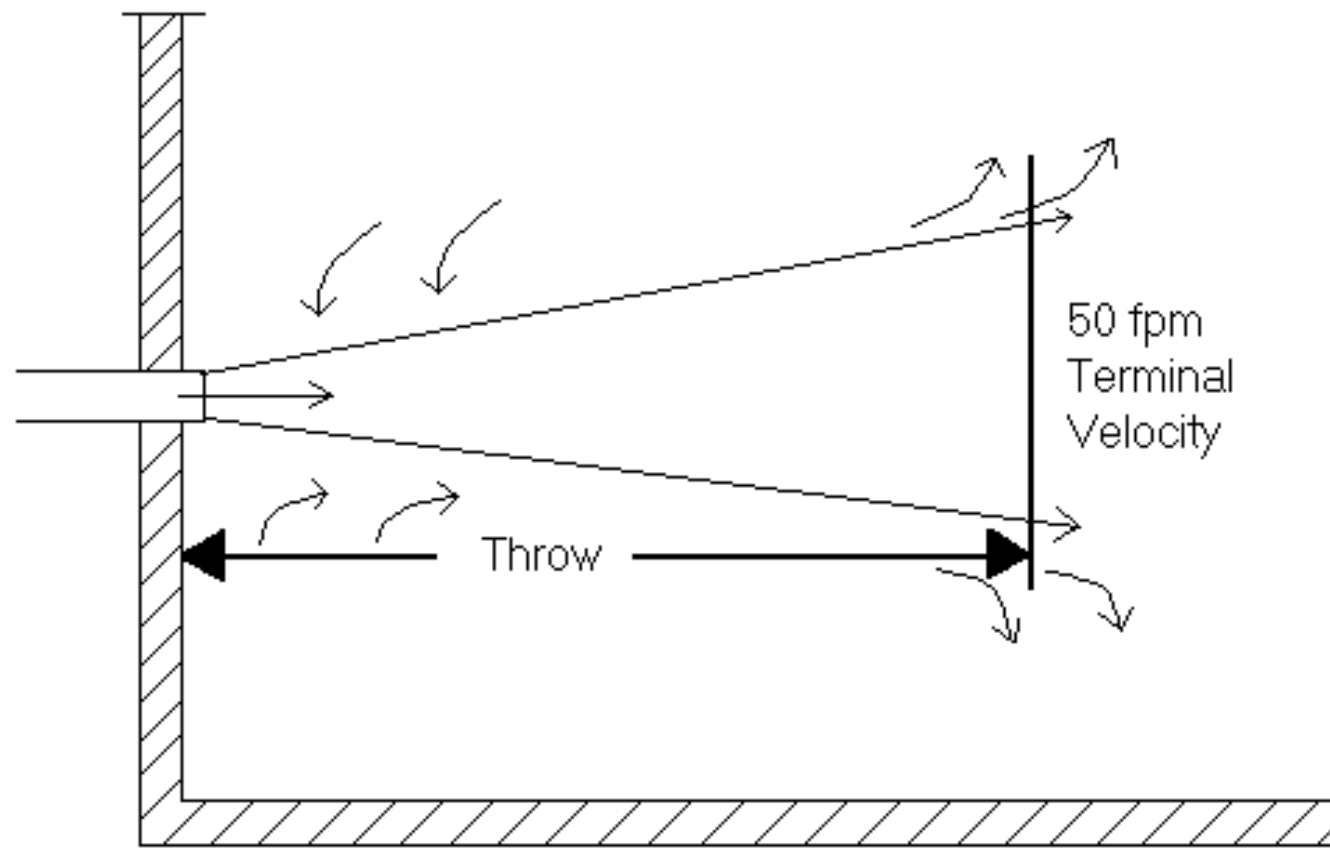
UP OUTSIDE WALL (HEATING)

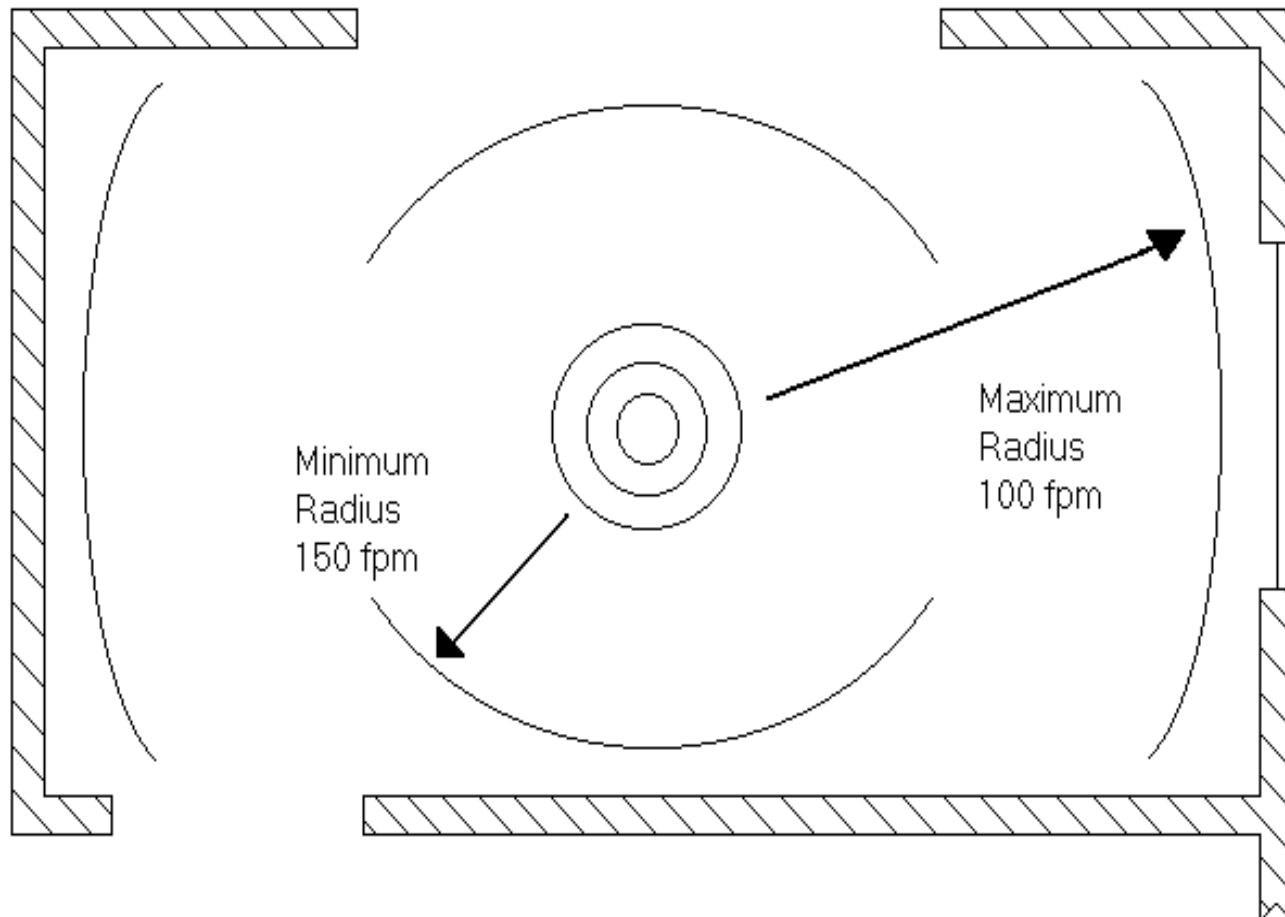
## CEILING

PARALLEL TO CEILING OUT TO  
WALLS  
(COOLING)

## HIGH INSIDE WALL

PARALLEL TO CEILING TO OUTSIDE  
WALL (COOLING)





# Returns – Adequate Air Pathways

Return Type	Advantages	Disadvantages
Single	<ul style="list-style-type: none"><li>■ Low Cost</li><li>■ Provides Accessible Filter Location</li><li>■ Low Surface Area</li></ul>	<ul style="list-style-type: none"><li>■ Potential for Inadequate Return Pathways (Pressure)</li><li>■ Potential for Noise</li></ul>
Every Room	<ul style="list-style-type: none"><li>■ Adequate Return Paths</li></ul>	<ul style="list-style-type: none"><li>■ High Cost</li><li>■ Excessive Duct Leakage</li><li>■ Unnecessary in Open Floor Plan</li></ul>

# Return Location

- **Mixing in a Room is Largely Unaffected by Return Location**
- **Return Location MAY Have a Small Effect on House Level Stratification**
- **House Level Stratification is More Affected by AC Size**



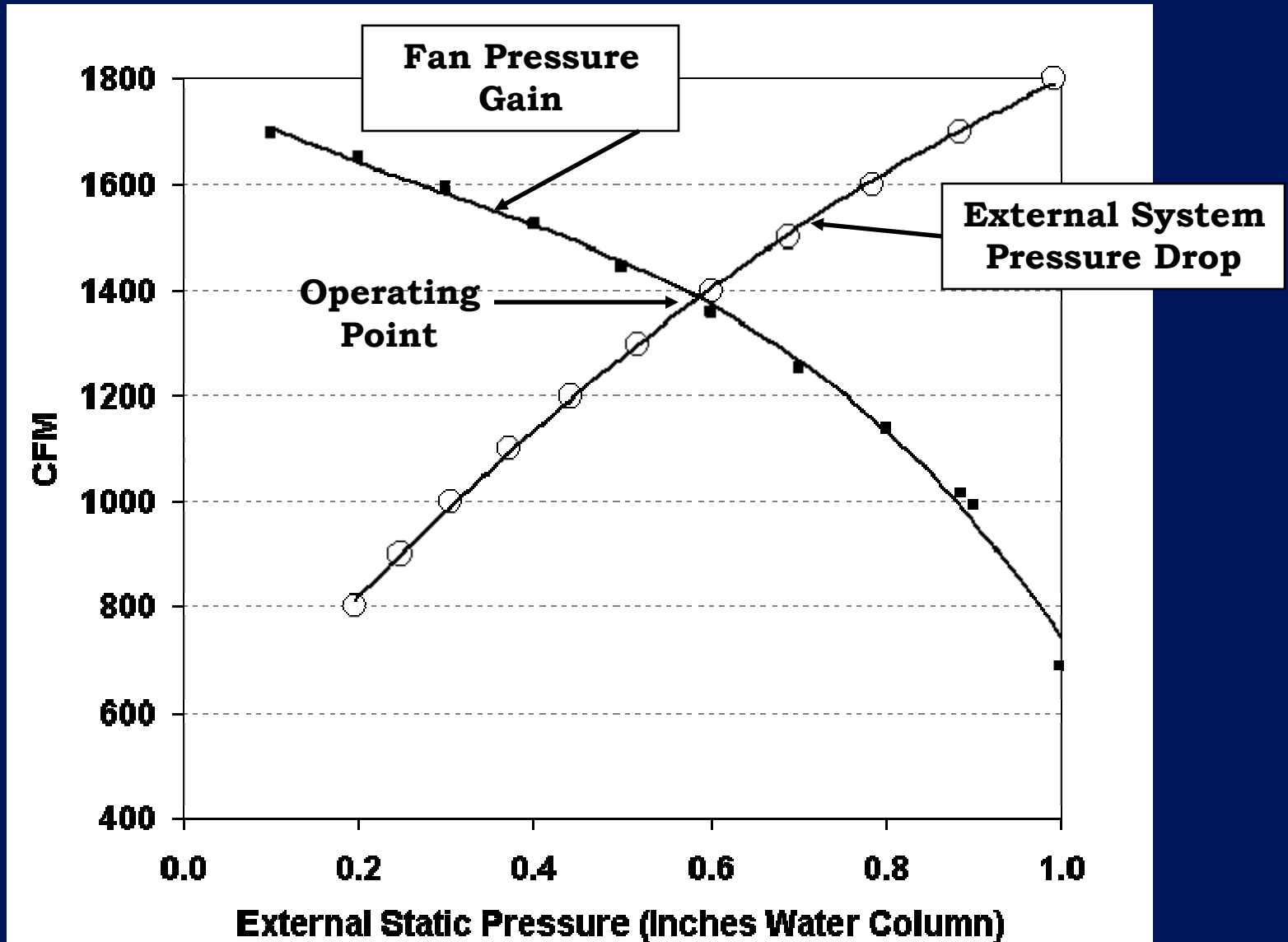
# Duct Design Considerations

WHAT DETERMINES FLOW THROUGH UNIT?

EXTERNAL SYSTEM      =      EQUIPMENT  
PRESSURE DROP                      PRESSURE GAIN

AT DESIRED FLOW

# External System Pressure Drop = Equipment Pressure Gain



# Generic External System Pressure Drops

<u>DEVICE</u>	<u>PRESSURE DROP</u>
Standard Filter	.10 Clean
High Efficiency Filter	.20 Clean
Humidifiers/Electric Heaters	.10 to .20
Supply Outlet	<u>.03</u>
Return Grille	<u>.03</u>
Balancing Damper	<u>.03 Open</u>
Coil	.15 to .45 wet coil
Duct System	<b><i>What is left</i></b>

# Coil Pressure Drop

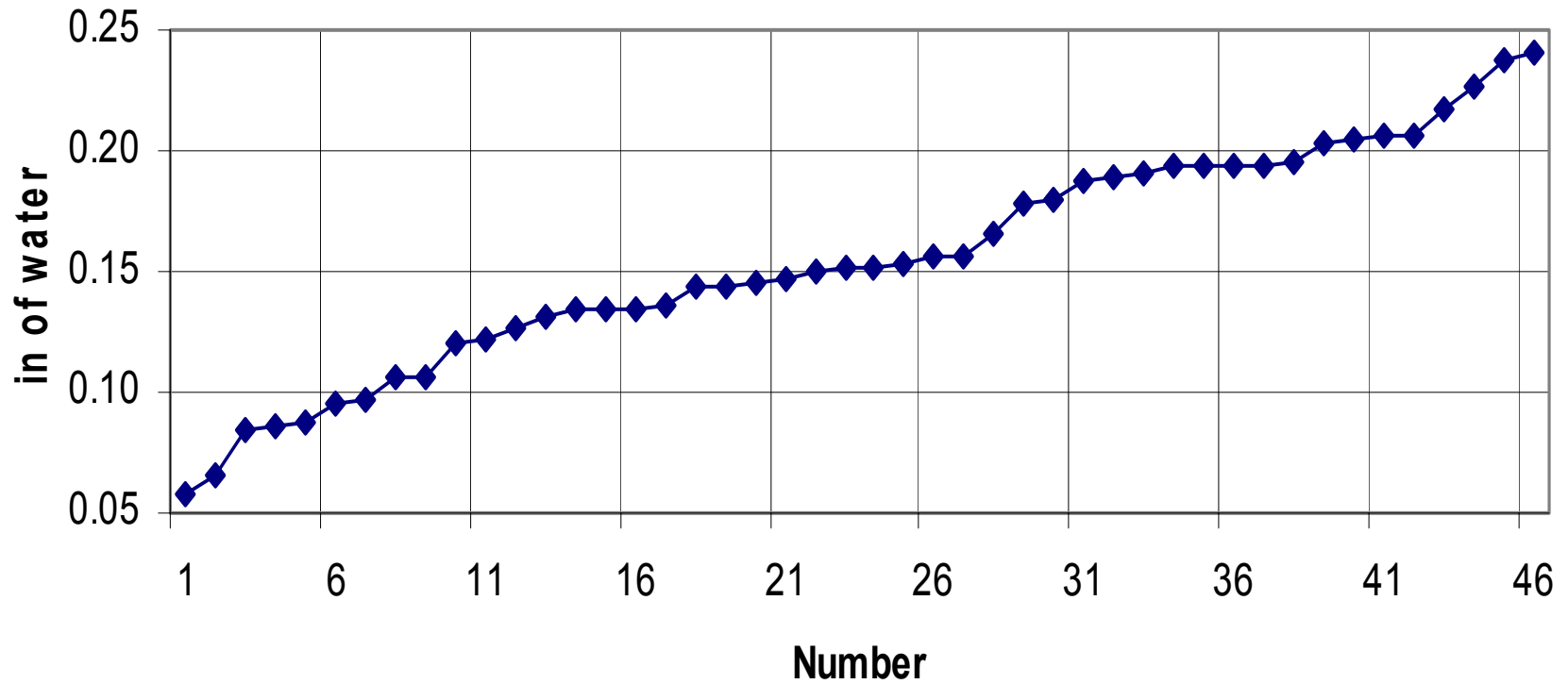


**G2FD036(S,H)21(T)**

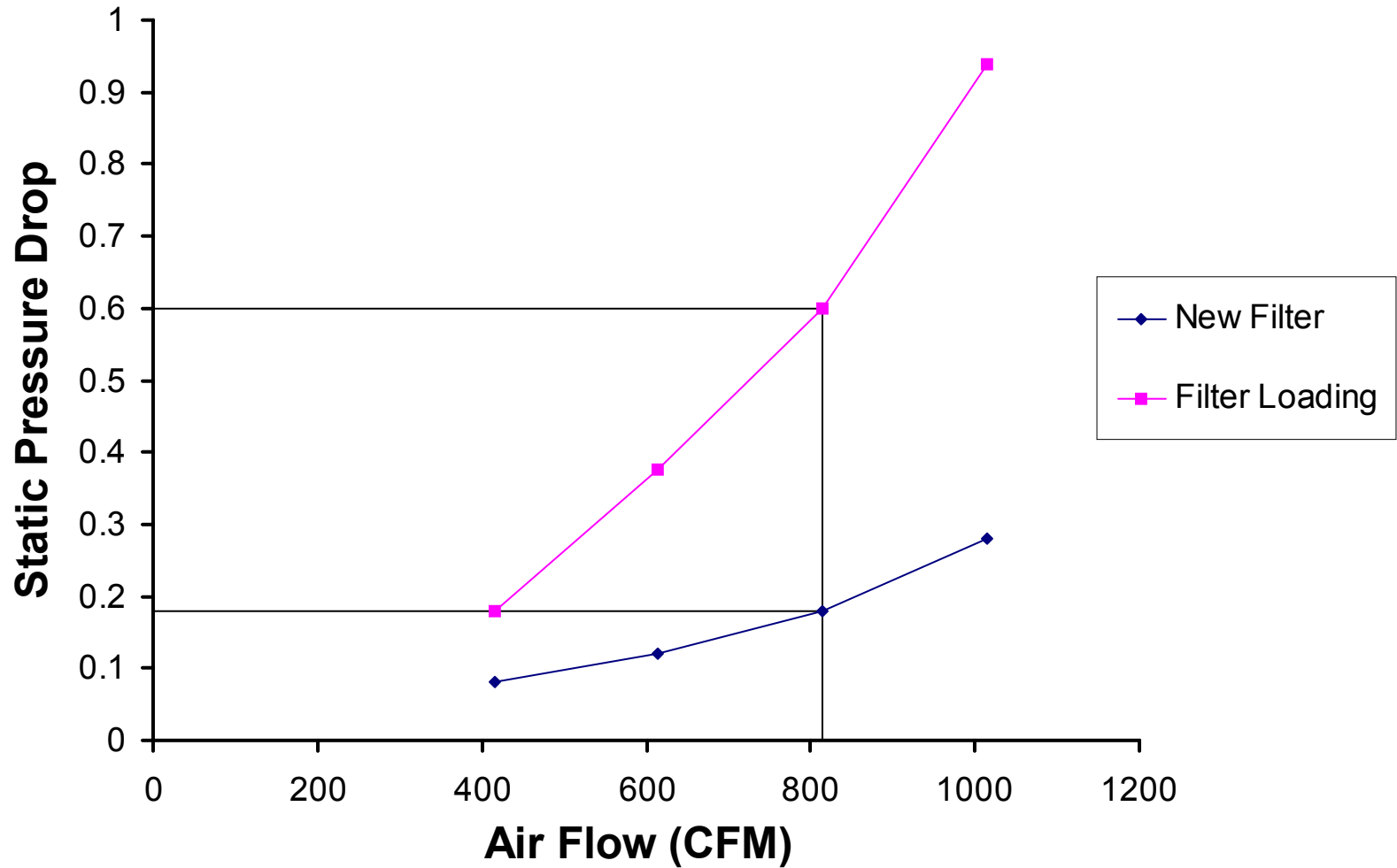
<b>CFM</b>	<b>Static Pressure (Wet Coil)</b>
<b>1000</b>	<b>0.23</b>
<b>1200</b>	<b>0.33</b>
<b>1400</b>	<b>0.45</b>

**Filter pressure drop is .05 – 0.24 in H<sub>2</sub>O**  
**Median is 0.15**

**Cooling Filter Pressure Drop**



# 20" X 20" MERV 8 Air Filter





<b>DX Coil Resistance (IWC)</b>		
<b>CFM</b>	<b>Dry</b>	<b>Wet</b>
1000	0.11	0.18
1200	0.15	0.26
1400	0.22	0.35
1600	0.28	0.46



<b>Electric Filter Resistance</b>	
<b>CFM</b>	<b>IWC</b>
1000	0.06
1200	0.08
1400	0.12
1600	0.15



<b>Heater Resistance</b>	
<b>CFM</b>	<b>IWC</b>
1000	0.09
1200	0.13
1400	0.18
1600	0.23

# Example Pressure Drop

<u>DEVICE</u>	<u>PRESSURE DROP</u>
Supply Register	.03
Return Grille	.03
Balancing Damper	.03
Coil	<u>.33 wet coil</u>

**Total EXCLUDING DUCTS** **.42**



# Equipment Pressure Gain

AIR DELIVERY—CFM (With Filter)\*

UNIT SIZE CARRIER	RETURN-AIR SUPPLY	SPEED	EXTERNAL STATIC PRESSURE (In. wc)							
			0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
060-12	1 side or bottom	High	1490	1450	1400	1345	1275	1190	1080	960
		Med-High	1190	1180	1155	1120	1070	1005	915	810
		Med	1015	1010	995	985	920	875	800	715
		Med-Low	870	860	840	820	780	735	670	580
		Low	685	670	645	620	595	545	495	420
080-12	1 side or bottom	High	1605	1560	1510	1450	1380	1300	1195	1045
		Med-High	1305	1290	1265	1225	1175	1100	995	895
		Med	1135	1125	1110	1080	1030	965	885	800
		Med-Low	990	980	965	930	880	825	760	685
		Low	805	780	745	700	660	630	575	495
		High	1810	1755	1690	1640	1565	1495	1410	1330
		Med-High	1420	1395	1350	1305	1260	1210	1145	1090

**.45 IWC at 1200 cfm**

# Cannot work – only .03 IWC available for duct system

WHAT DETERMINES FLOW THROUGH UNIT?

EXTERNAL SYSTEM      =      EQUIPMENT  
PRESSURE DROP                      PRESSURE GAIN

**0.42 IWC +                      0.45 IWC**  
**Ducts**

AT DESIRED FLOW

**1200 cfm**

# Stick with Smaller Air Handler – Smaller Fan Motor



## Performance data

UNIT SIZE	060-12	080-12	080-16
DIRECT-DRIVE MOTOR Hp (PSC)	1/3	1/3	1/2
MOTOR FULL LOAD AMPS	5	5	7.4
RPM (Nominal) — SPEEDS	1075—5	1075—5	1075—5
BLOWER WHEEL DIAMETER X WIDTH (In.)	10 x 7	10 x 7	11 x 8
FILTER SIZE (In.) — (Washable)	(1) 16 x 25 x 1		

PSC—Permanent Split Capacitor

# Solution

- Keep smaller air handler
- Use a less restrictive coil (0.21 IWC)
- Drop the dampers
- External system pressure drop becomes:
  - Return Grille .03
  - Supply Register .03
  - Coil .21
  - TOTAL .27 + Ducts
- Equipment Pressure
  - at Med. Hi and 1200 cfm 0.45
- Available for ducts  $0.45 - 0.27 = 0.18$

# Now we need to know the friction rate (IWC/100 ft.)

- We have an available static pressure of 0.18 Inches of Water Column
- What do we want to divide that by to get the friction rate?

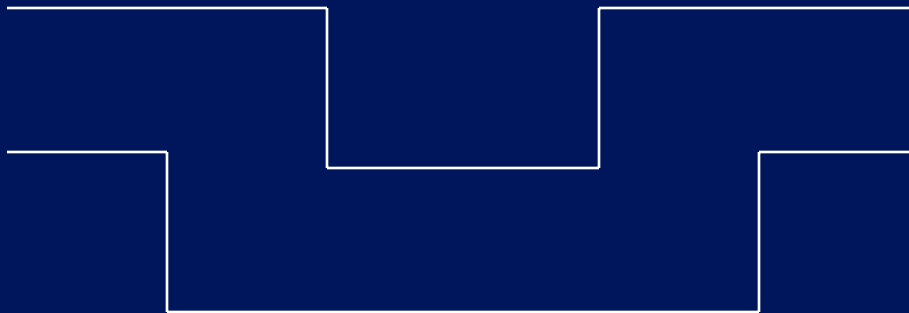
**The Total Effective Length**

# How Long is the Duct System? (from an air molecule's view)

- A 200 ft. straight pipe is 200 feet long



- This 4 ft. section of pipe is how long?

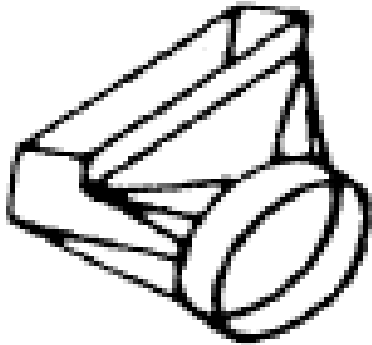


330 FEET

# Supply Boots

4 - G

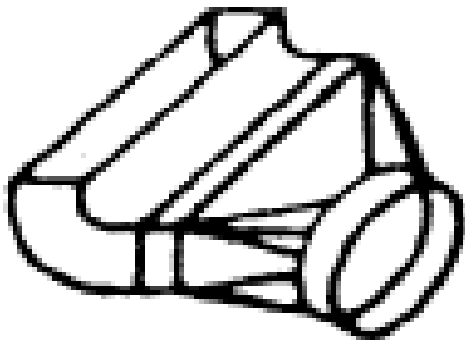
EL = 80



**4-G**

4 - J

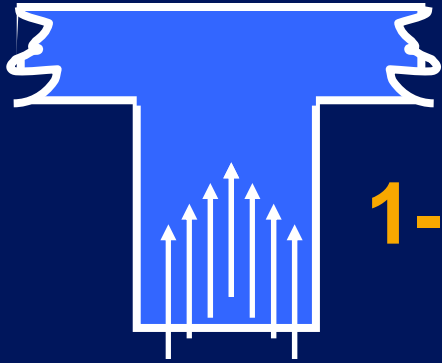
EL = 30



**4-J**

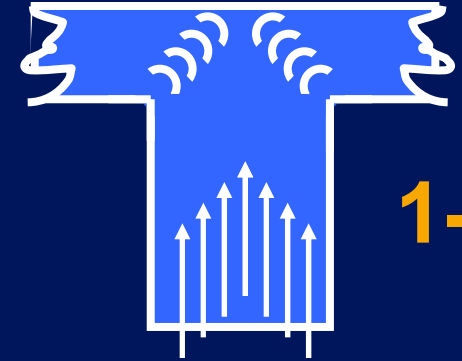
Fitting Number	Effective Length
4-G	80 ft.
4-J	30 ft.

# Supply Plenums and Takeoffs

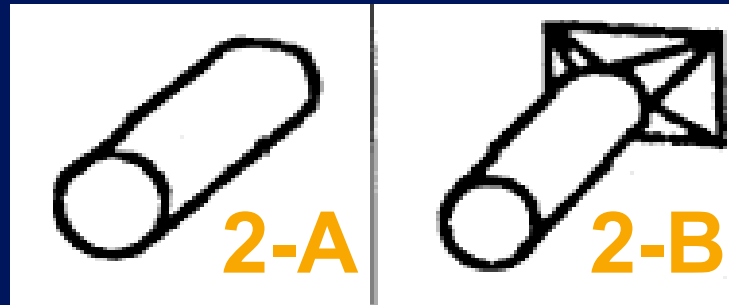


**1-O**

Fitting Number	Effective Length
1-O	60 ft.
1-P with Vanes	40 ft.



**1-P**



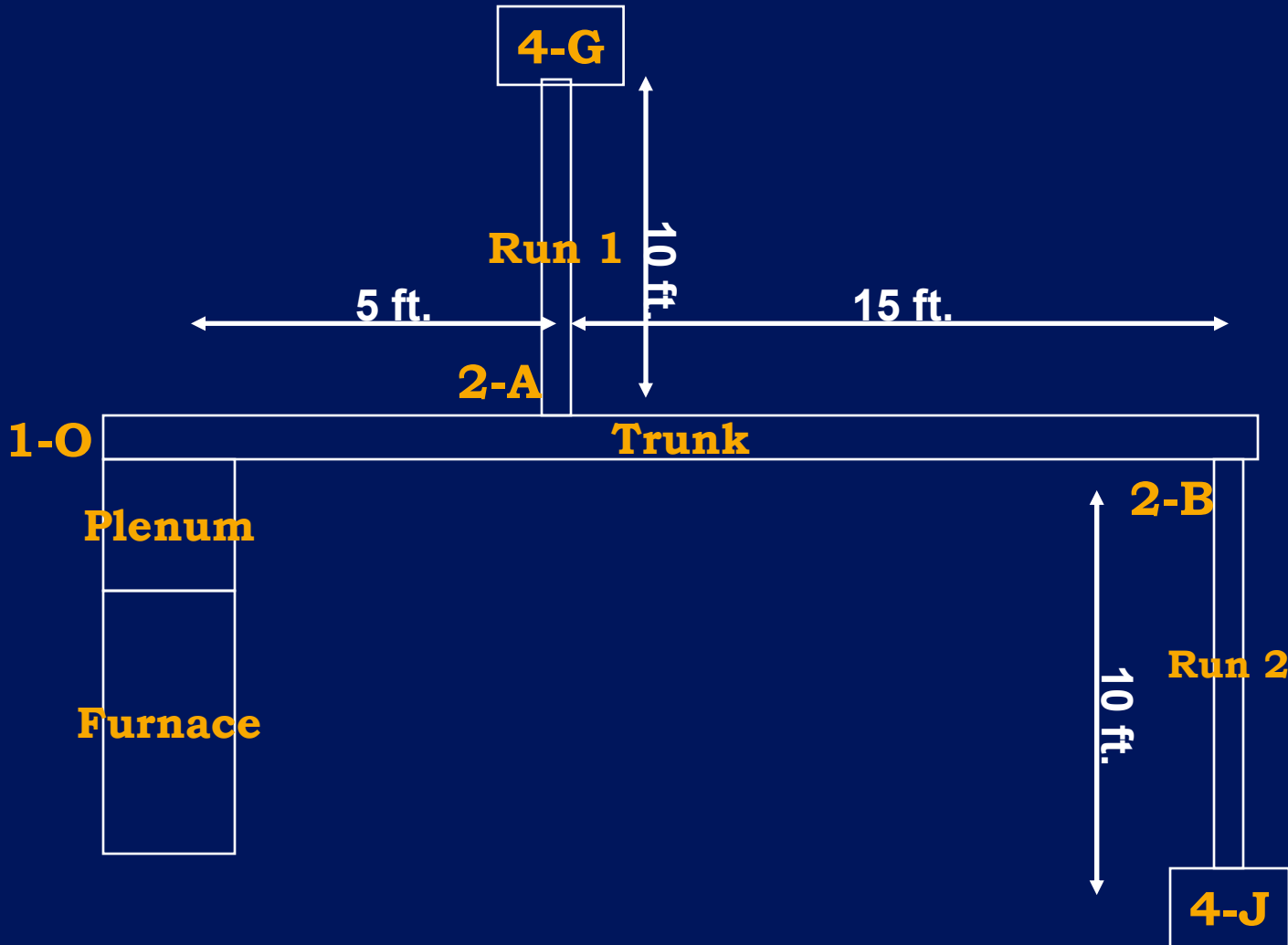
**2-A**

**2-B**

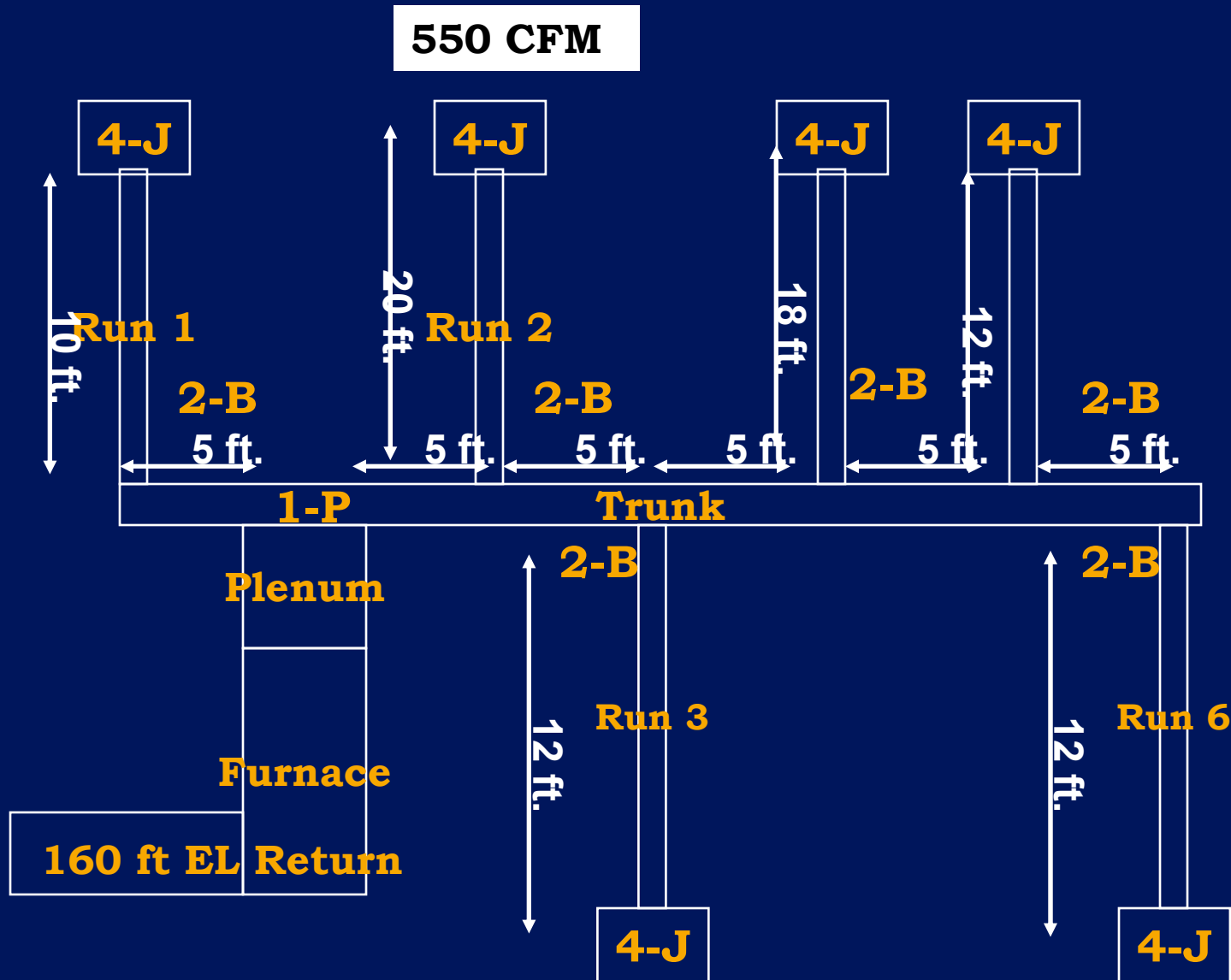
Downstream Branches	0	1	2	3	4	5 or +
2-A	35	45	55	65	70	80
2-B	20	30	35	40	45	50



# A Simple Duct Design



# A Less Simple Duct Design



**90 CFM**

# Calculate the Total Effective Length from the return grille to the supply register

- A simple takeoff can be as little as 10 feet

**Or as much as 115 feet**

- Through good design we got the overall equivalent length to 300 feet

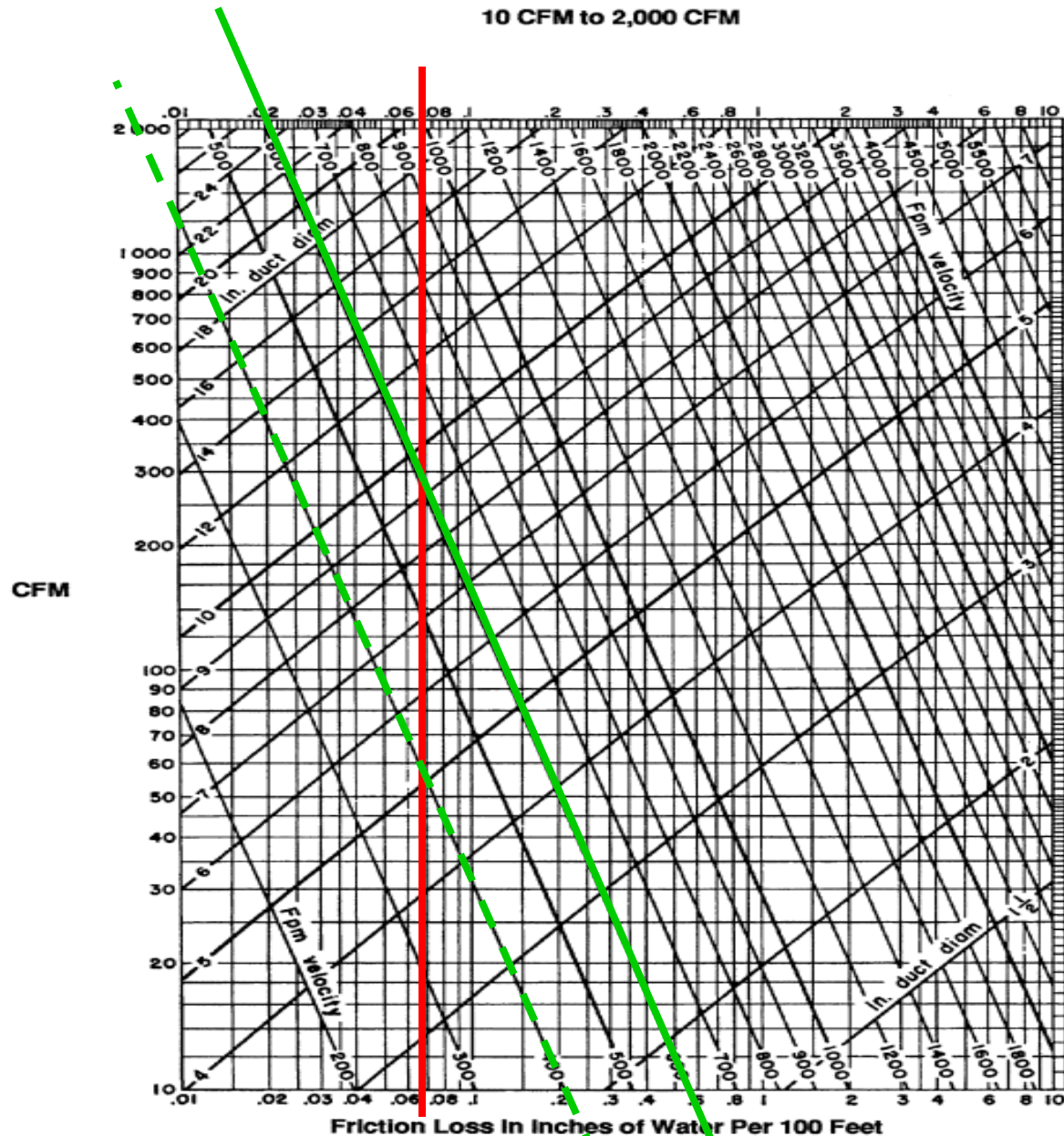
- So we have 0.18 IWC available static pressure over 300 ft.

The friction factor is .06 IWC per 100 ft  
( $0.18/300 = 0.06$ )

# Chart 1

## Round Galvanized Metal Duct

### 10 CFM to 2,000 CFM



**Notes:**

- 1) Correction required for nonstandard air
- 2) 40 joints per 100 feet
- 3) Roughness = 0.0005 feet

# Recommended Velocity (in fpm)

Duct Type	Supply		Return	
	Rigid	Flex	Rigid	Flex
Trunk	700	600	600	600
Branch	600	600	400	400
Outlet	Size for Throw			
Return Grille Face			<500	
Filter Grille			<300	

# Why not just use 0.10 IWC /100 ft. Friction Rate on a Ductalator?

BECAUSE

- DESIGN VALUE FOR FRICTION RATE IS NOT ARBITRARY
- FRICTION RATE DESIGN VALUE DEPENDS ON AVAILABLE STATIC PRESSURE AND TOTAL EFFECTIVE LENGTH

# Desirable Design

- **SHORT DUCT RUNS**
- **LOW STATIC PRESSURES**
- **INSIDE CONDITIONED SPACE**
- **GOOD THROW ON REGISTERS**

# Duct Installation

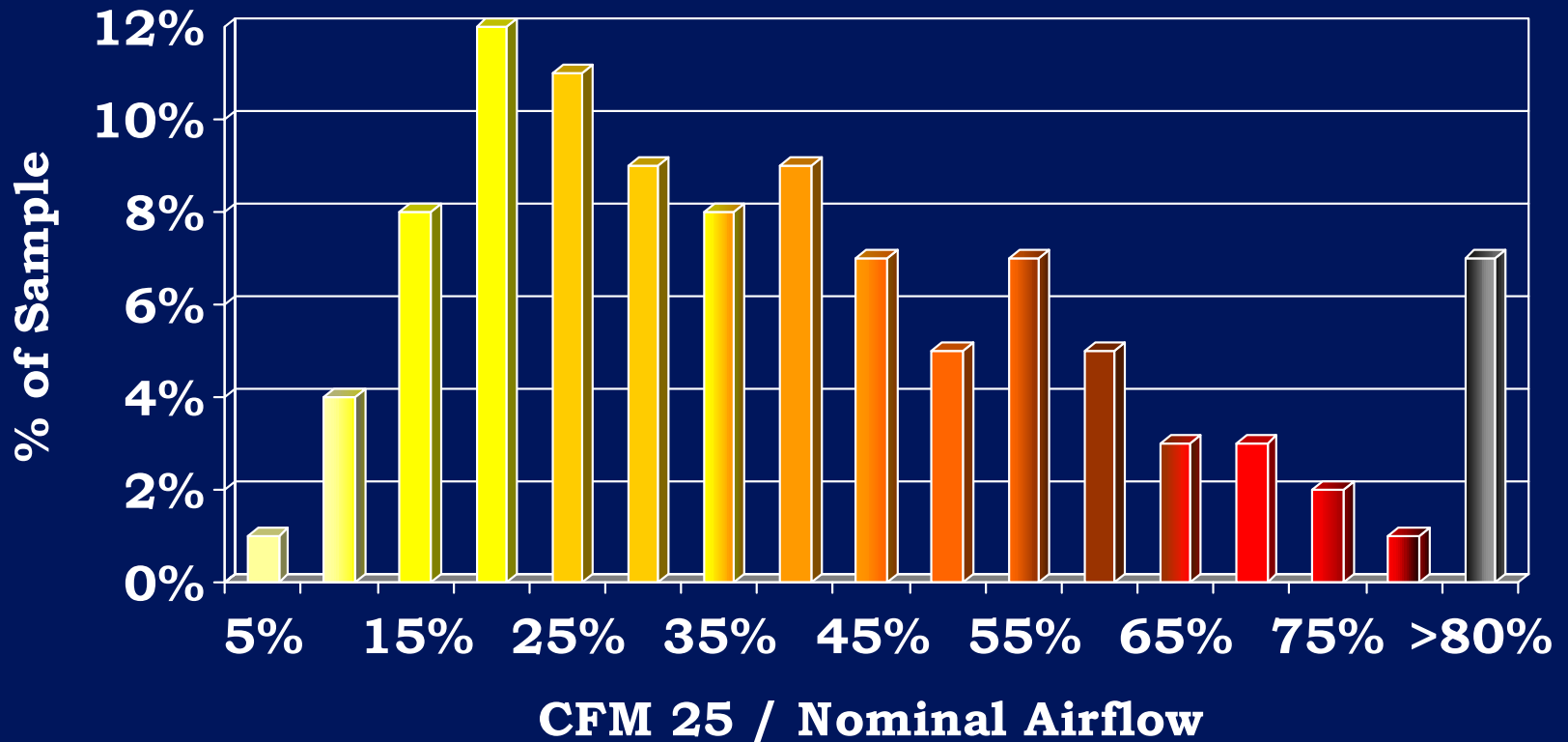
- Put in what is designed
- Straight
- Leakless
- Proper Flow
- Proper Distribution



# Duct Testing

- Leakage
- Flow
- Distribution

# Duct Leakage in Existing Homes



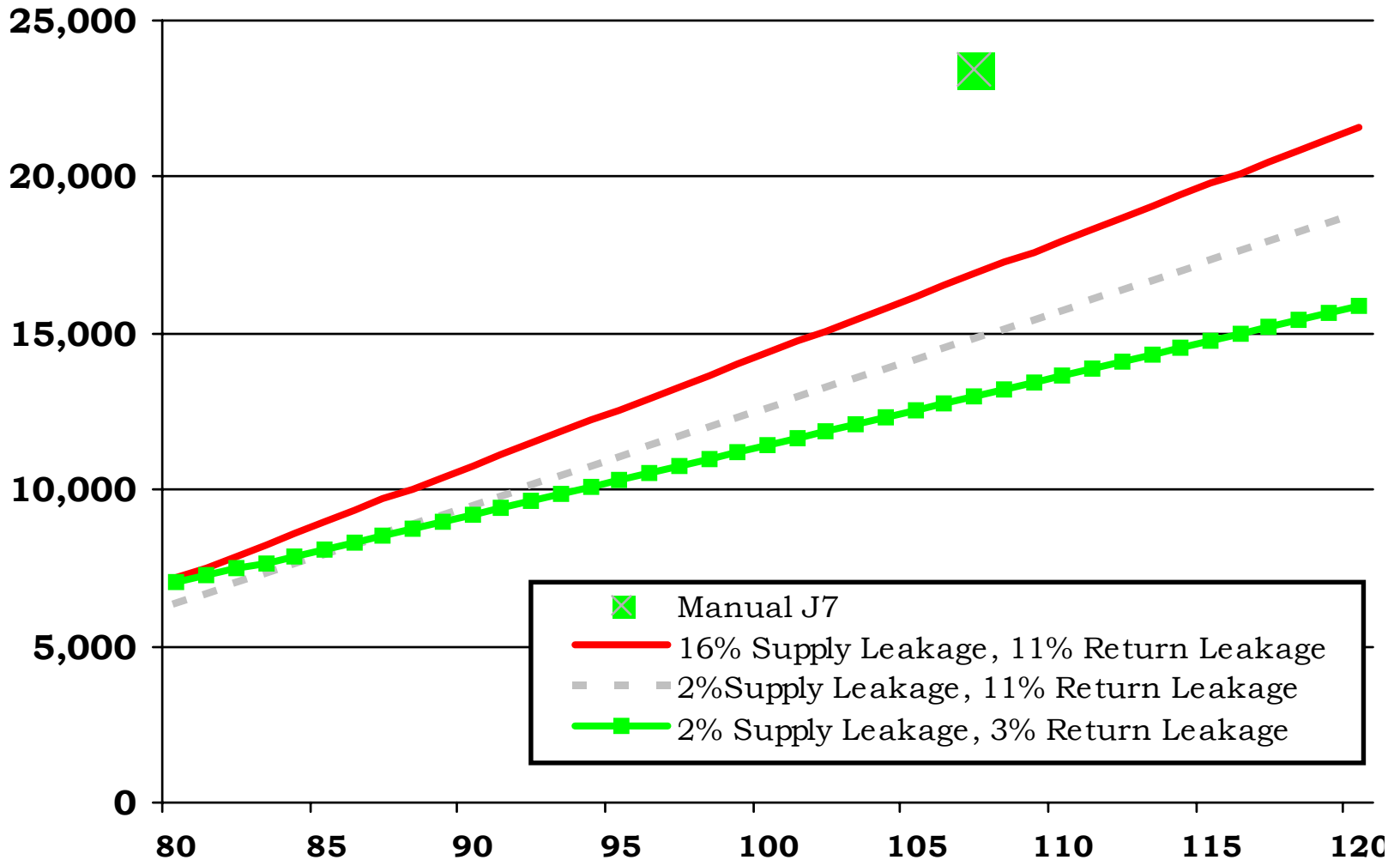
Sample size: 1210 (no mobile homes)

Test method: Duct Blaster® at 25 pa. (0.10"WC)

Source: CheckMe!® database

# Duct Sealing Saves Energy and Peak

Required Sensible Cooling (BTUh)



# DUCT LEAKAGE TESTING

- Total Leakage
- Leakage to Outside
- Supply Side Leakage
- Return Side Leakage
- Operating Leakage

# TOTAL LEAKAGE SET-UP

- REMOVE FILTERS
- MOUNT DUCT BLASTER™ @ AH OR RETURN GRILLE
- ALL SUPPLY REGISTERS COVERED
- ALL RETURN GRILLES COVERED
- DUCT TEST REFERENCE PRESSURE IN SUPPLY PLENUM (STATIC PRESSURE PROBE)

# Duct Blaster® Test Method



- MEASURE CFM TO KEEP DUCTS AT 25 PA
- MEASURE CFM TO KEEP DUCTS AT 25 PA

# DUCT TESTING PROCEDURE

- KEEP FAN PRESSURE ABOVE 30 PASCALS  
(SWITCH FLOW RING IF NEEDED)

- FLOW RING SELECTION

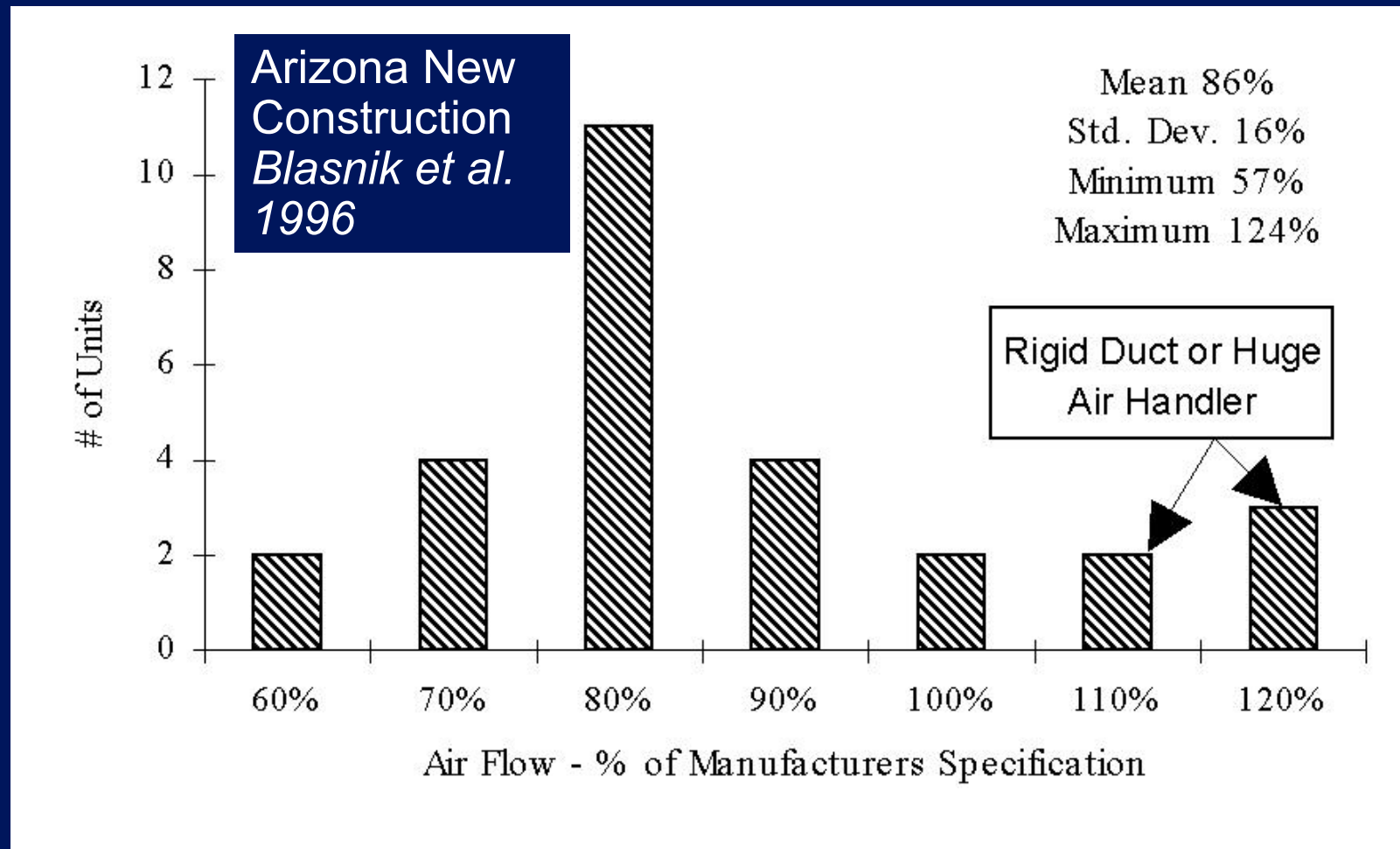
- OPEN 1,500 TO 500
- RING 1 800 TO 200
- RING 2 300 TO 75
- RING 3 125 TO 30

# Duct Leakage Standards

- CFM 25 as % of Cooling Nominal Flow
  - Nominal Flow as 400 CFM per ton
  - 5%, 6%, 8%
- CFM 25 as % of Actual Flow
- CFM 25 as % of Floor Area



# Low Airflow



- All of the audited forced air systems showed low air handler flow  
*Danny Parker Florida Study 1997*

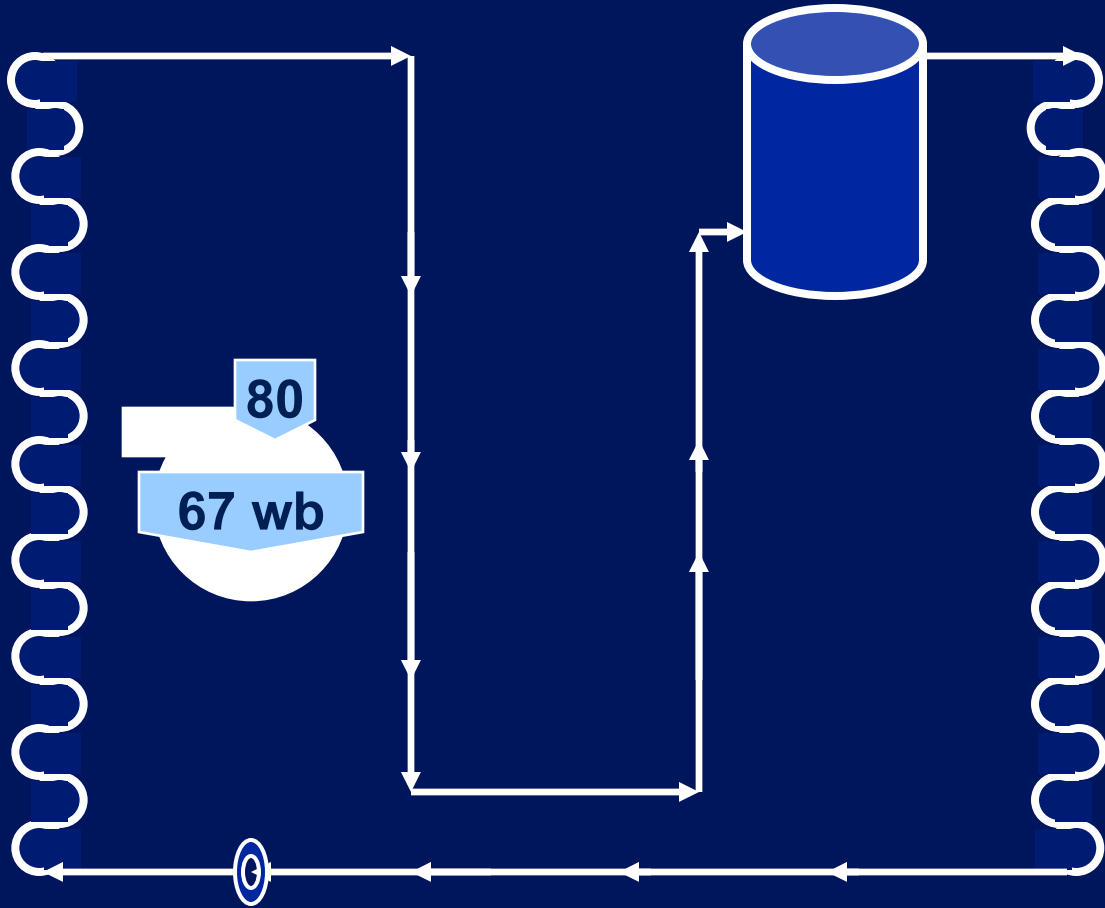
# Measuring Airflow

- Temperature Split Method
- **Duct Blaster™**
- **Flow Capture Hood**
- **Flow Grid**
- Coil Pressure Drop
- Fan Curve
- Pitot Tube Traverse
- Anemometer

# AC Temperature Split

- Run to steady state (15 minutes)
- Measure return “wet bulb” and dry bulb temperatures
- Measure the supply dry bulb temperature
- This is the most critical part of the procedure
  - System stabilized
  - The measured temperatures as close to the mixed **PLENUM AIR TEMPERATURES**

55



# Determining Target Temperature Split

- Target temperature split is not constant
  - Target temperature split varies with
    - Return dry bulb
    - Return wet bulb
- Determine the target temperature split
  - Based on chart or “slide rule”

# Maximum Temperature Split Table

Return Air Dry-Bulb (°F)	Return Air Wet-Bulb (°F)													
	50	52	54	56	58	60	62	64	66	68	70	72	74	
70	23.9	23.6	23.1	22.5	21.7	20.7	19.5	18.2	16.7	14.9	13			
72	24.9	24.7	24.2	23.6	22.8	21.8	20.6	19.3	17.7	16	14.1	12		
74	26	25.8	25.3	24.7	23.9	22.9	21.7	20.4	18.8	17.1	15.2	13.1		
76	27.1	26.9	26.4	25.8	25	24	22.8	21.5	19.9	18.2	16.3	14.2	11.9	
78	-	-	27.5	26.9	26.1	25.1	23.9	22.5	21	19.3	17.4	15.3	13	
80	-	-	-	28	27.2	26.2	25	23.6	22.1	20.4	18.5	16.4	14.1	
82	-	-	-	-	28.2	27.2	26.1	24.7	23.2	21.5	19.6	17.5	15.2	
84	-	-	-	-	-	28.3	27.2	25.8	24.3	22.5	20.6	18.6	16.3	

# TrueFlow™ Flow Grid



# Grid Installs in Filter Slot





# Duct Blaster® Test Method



- Take supply static pressure with air conditioner running
- Block blower compartment from return system
- Install Duct Blaster® on the blower compartment door
- Turn on air handler
- Adjust Duct Blaster® speed to duplicate supply static
- Read airflow from Duct Blaster®

# Desired Air Flow

SHR	CFM per Ton
Below 0.74	300
0.74 to 0.79	350
0.80 to 0.85	400
Above 0.85	450

# Flow to Rooms

- Within  $\pm 10\%$
- $\pm 20\%$  Max.

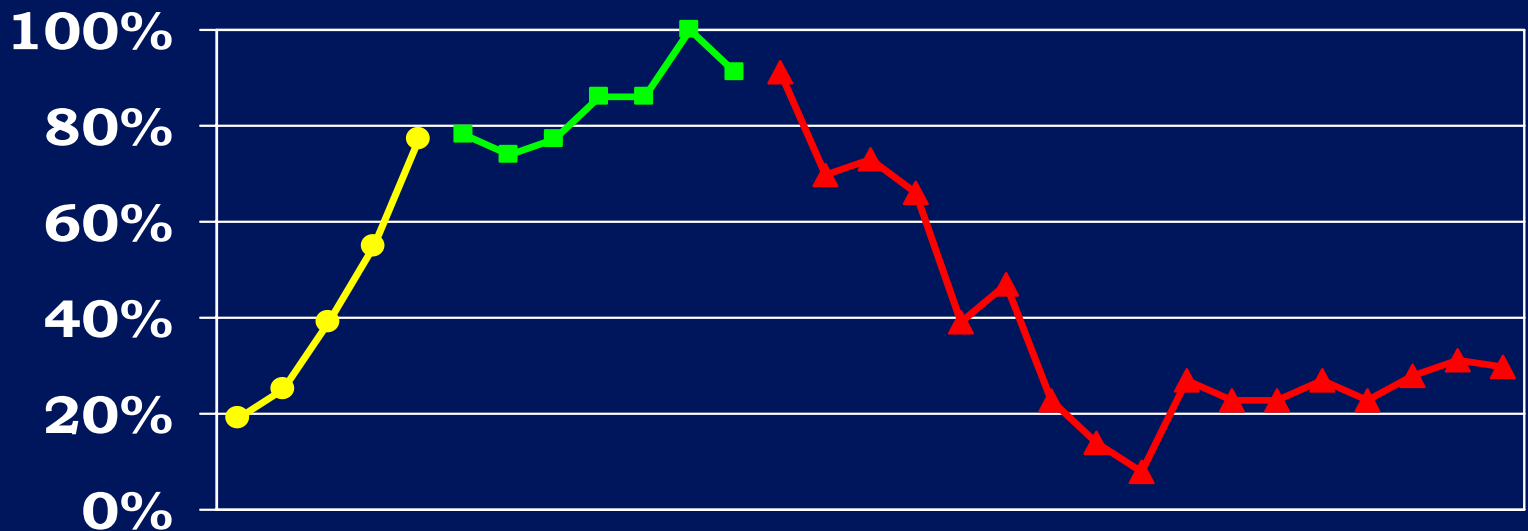
# **Write the Specifications Sign the Contract Breathe Easy --- NOT**

- Any equipment installed must perform as intended

**These items are accomplished by  
human beings and are subject to error.**

**With Initial Feedback the Crews Learned Rapidly.  
With Continued Feedback They Maintained Good  
Savings  
When Feedback Was Removed the Savings Dropped  
to 30% of the Maximum**

**Measured Savings  
as a Percent of Achievable Savings  
(running average)**



- Program Startup, Learning Curve with Technician Feedback**
- Production with Feedback Maintained**
- ▲ Disaster when Feedback was Removed**